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INTRODUCTION

The L'Aquila earthquake (Mw 6.3) occurred on April 6th at 01:32 UTC in the Central Appennines at a depth of about 9 km and was felt all over Central Italy. The main shock was preceded by a long seismic sequence started several months before and was followed by thousands of aftershocks, some of them with Mw>4.

In the present work we computed the coseismic deformation field induced by the earthquake by means of a 3D Finite Element (FE) analysis. To this effort we implemented different seismic source models obtained from fault inversion of GPS measurements, joint inversion of strong motion and GPS data and joint inversion of DInSAR displacements and GPS data.

COMPUTATIONAL TOOLS

The model was built and meshed by means of **CUBIT**, from Sandia National Laboratories (<http://cubit.sandia.gov/index.html>), a powerful and full-featured software toolkit for robust generation of two- and three-dimensional FE grids and geometry preparation.



The FE simulation was carried out by **FEMSA**, a recently developed FE simulation tool (Volpe et al. 2007). It is based on **CalculiX**, (<http://www.calculix.de/>), a free package designed to solve field problems.

FEMSA
Finite Element Modeling
for Seismic Applications

The main features of simulating with FEMSA are:

- the seismic source is implemented as a suitable distribution of double couples of forces
- arbitrary fault geometry and slip distribution are allowed
- inhomogeneous boundary conditions are applied by prescribing analytically computed displacements to the edge nodes (Okada model).

M. Volpe, D. Maffei, A. Piersanti, FEMSA: a finite element simulation tool for quasi-static seismic deformation modeling, *Annals of Geophysics* (2007), 50, 367

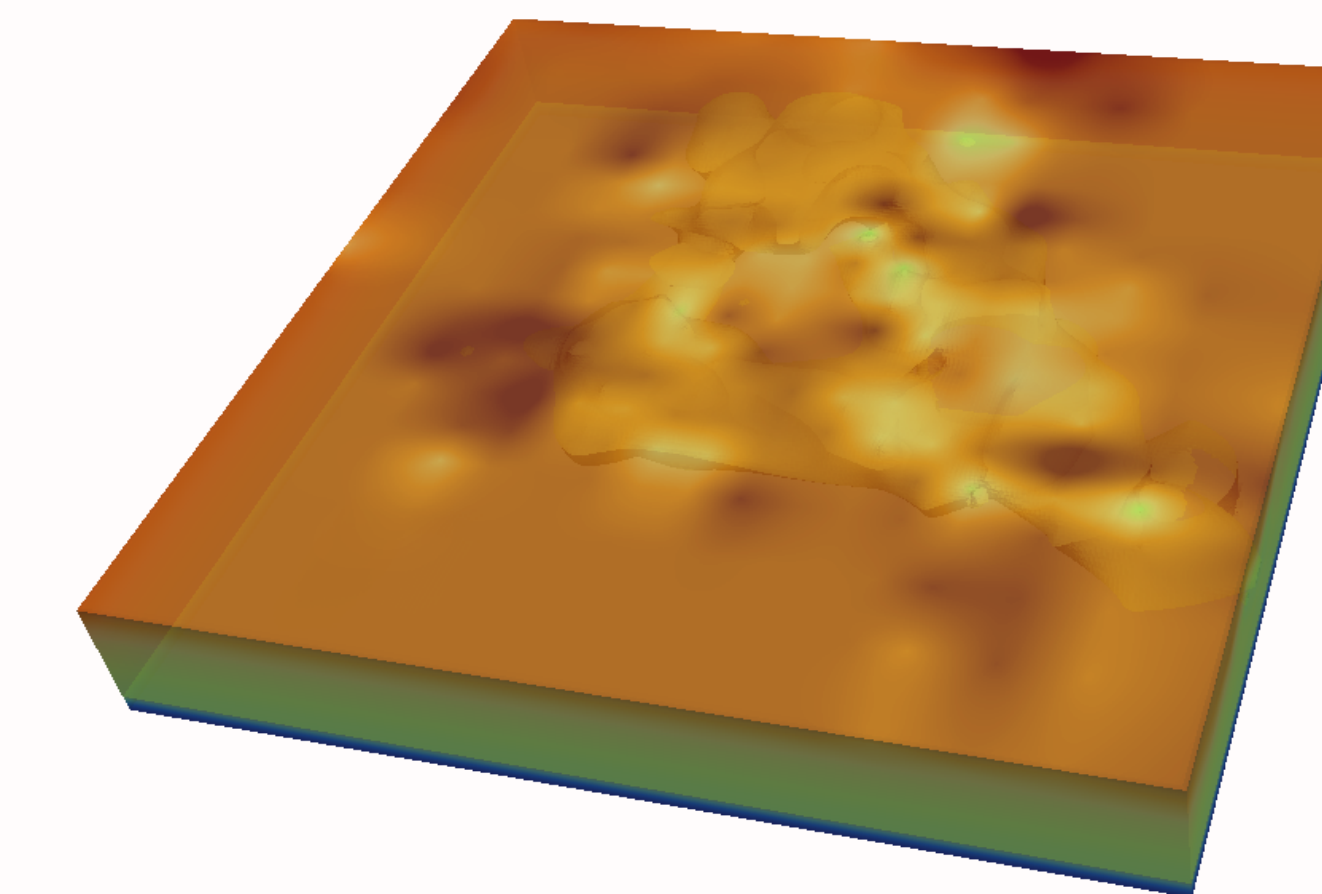
THE MODEL

We built up a **high-resolution three-dimensional** flat model ~20 km thick spanning a surface of about 13500 km² in the Central Italy.

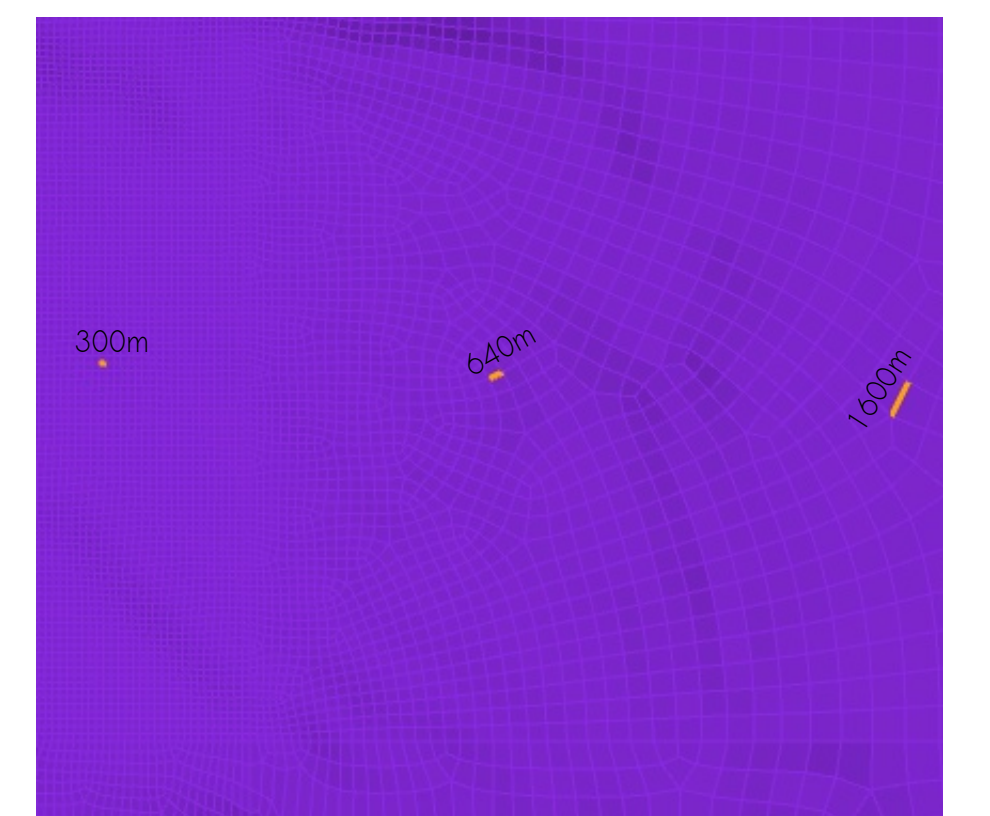
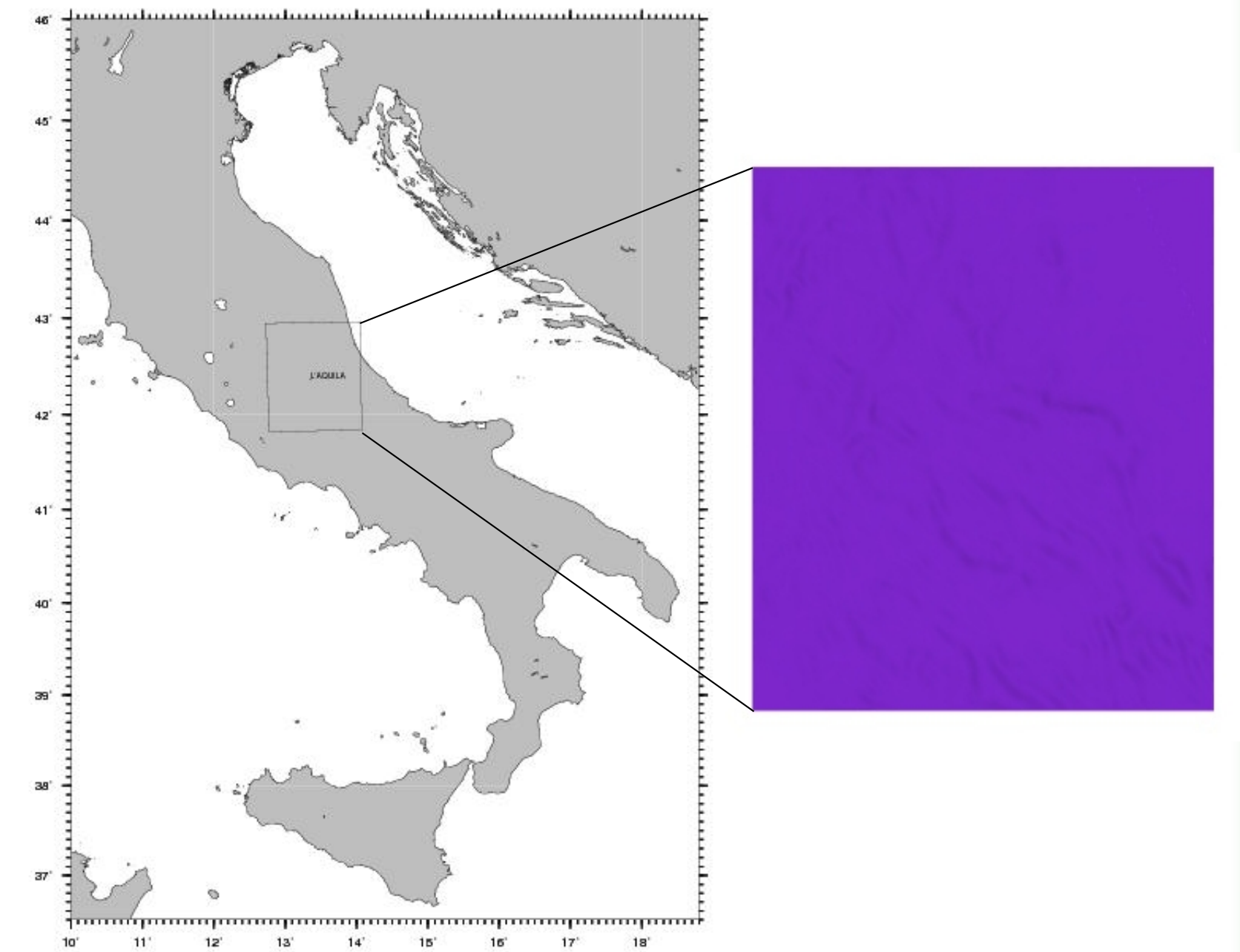
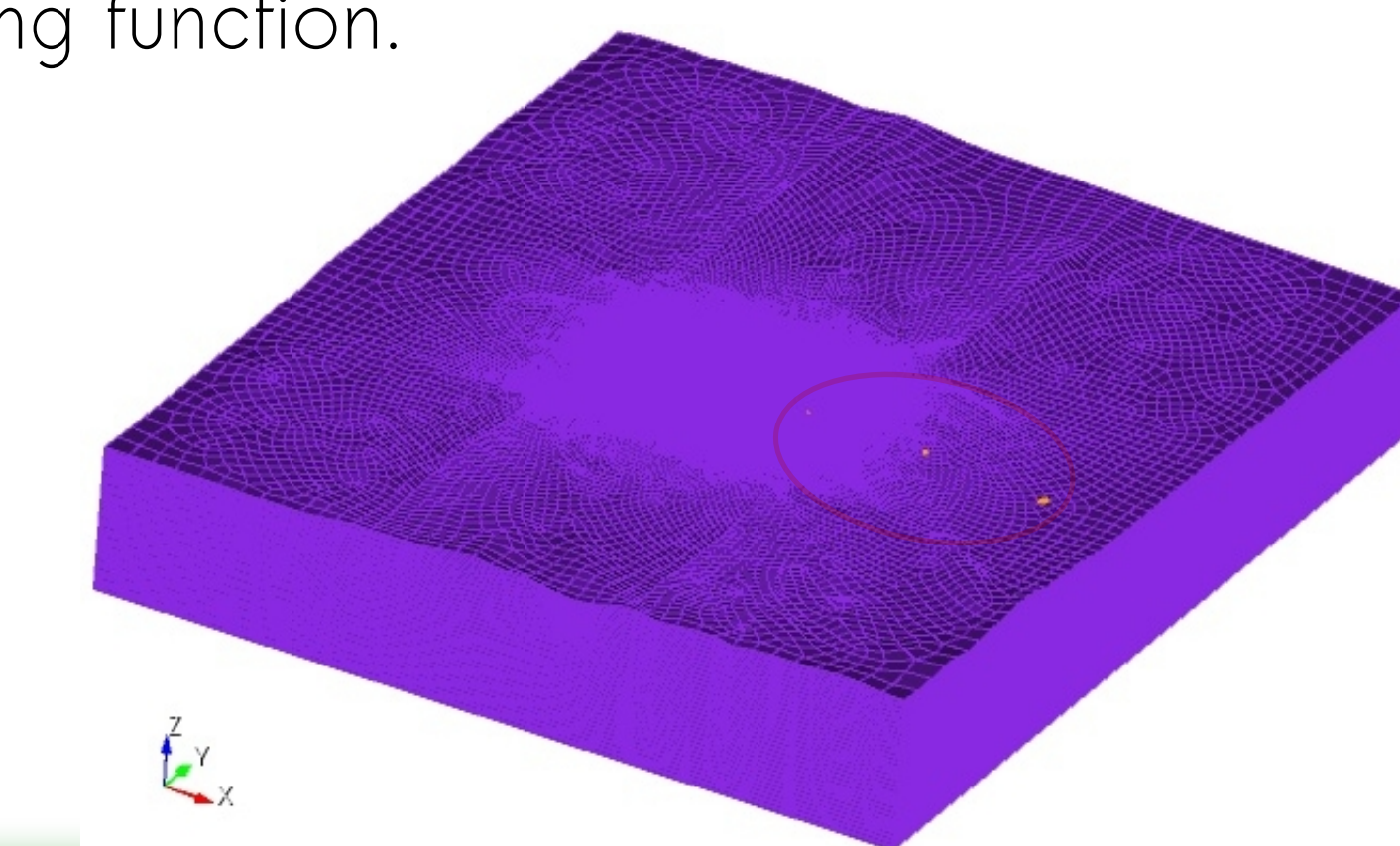
Surface **topography** having **500m** spatial resolution has been incorporated within the model.

The rheological properties of the domain were deduced from a vp/vs travel time **tomographic model**.

The domain was discretized using 20-nodes brick elements. The generated unstructured mesh contains 1461474 elements, resulting in 5933380 nodes. The element horizontal size is biased from 300m to 2-3km using the paving meshing algorithm in combination with an appropriate adaptive sizing function.



The tomographic model from De Gori et al (2010).



A detail of the mesh biasing

SOURCE MODELS

FAULT PLANE WITH HOMOGENEOUS SLIP DISTRIBUTION
from inversion of GPS data (Anzidei et al. 2009)

strike angle=141.6°
dip angle=54.5°
rake angle=-93.8°

1

FAULT PLANE WITH HETEROGENEOUS SLIP DISTRIBUTION
from joint inversion of strong motion and GPS data (Cirella et al. 2009)

strike angle=133.°
dip angle=54.°
rake angle= variable

2

FAULT PLANE WITH HETEROGENEOUS SLIP DISTRIBUTION
from inversion of DInSAR coseismic displacements (Atzori et al. 2009)

strike angle=133.5°
dip angle=47.°
rake angle=-103.5

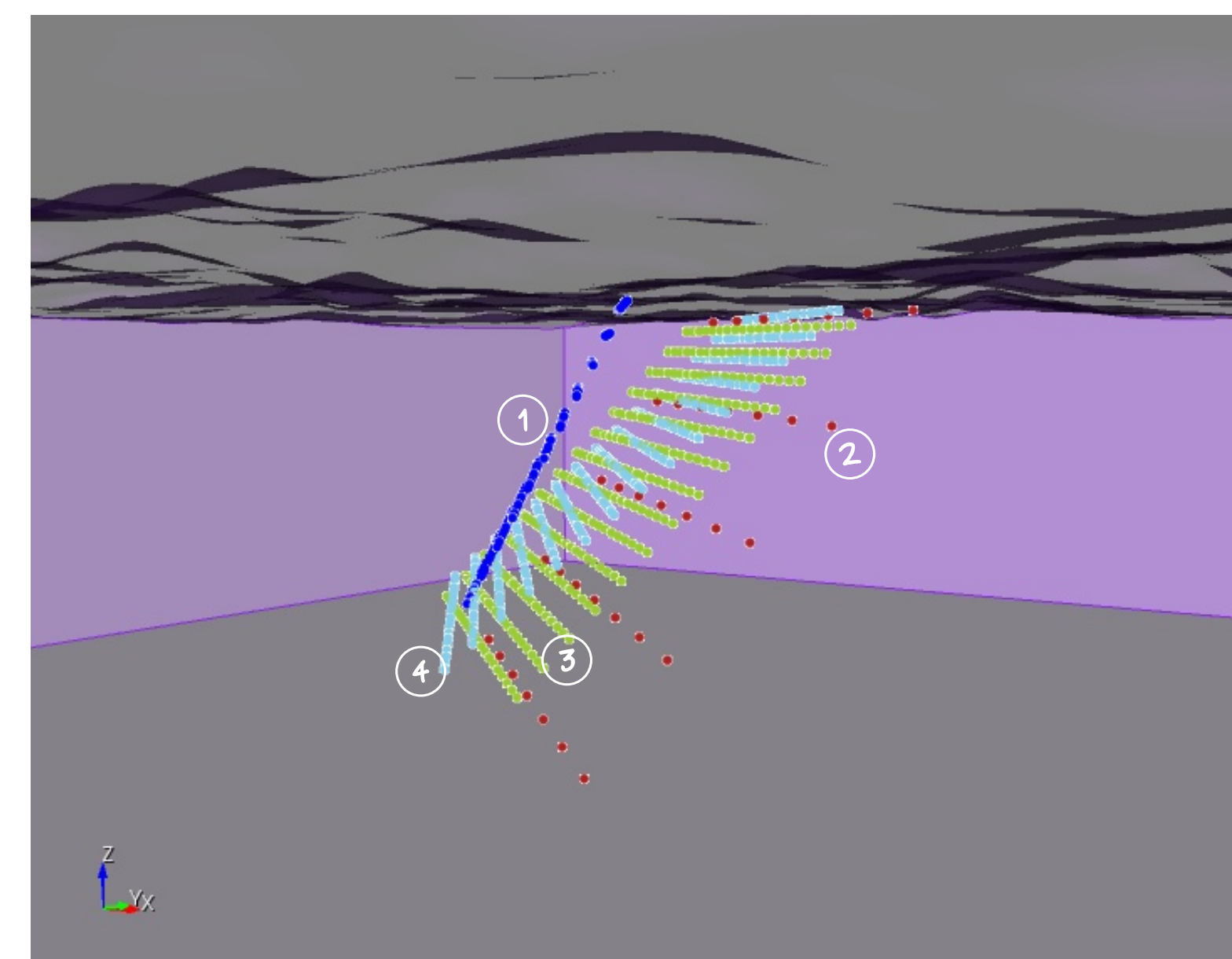
3

FAULT PLANE WITH HETEROGENEOUS SLIP DISTRIBUTION
from inversion of DInSAR coseismic displacements (Trasatti et al. 2009)

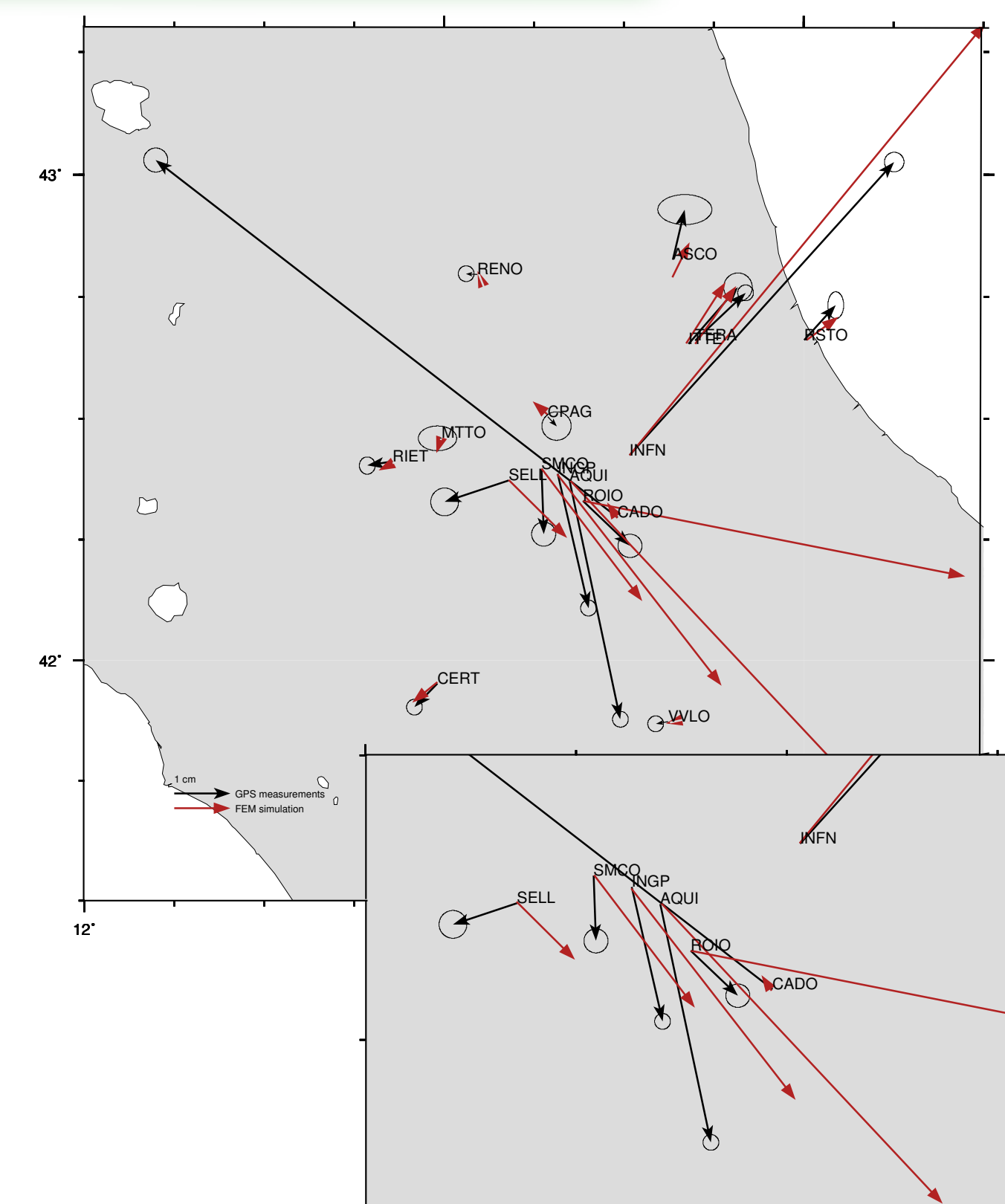
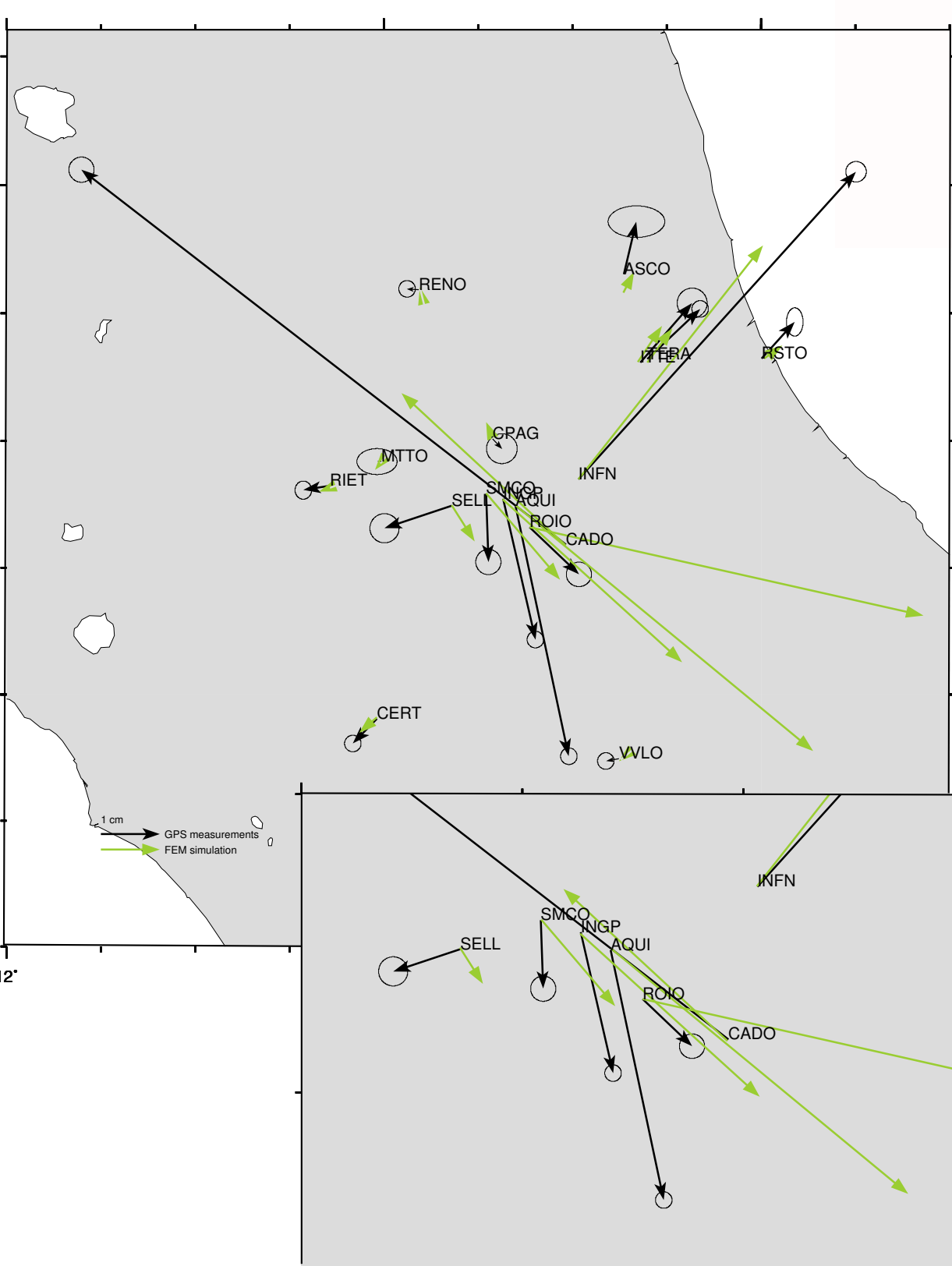
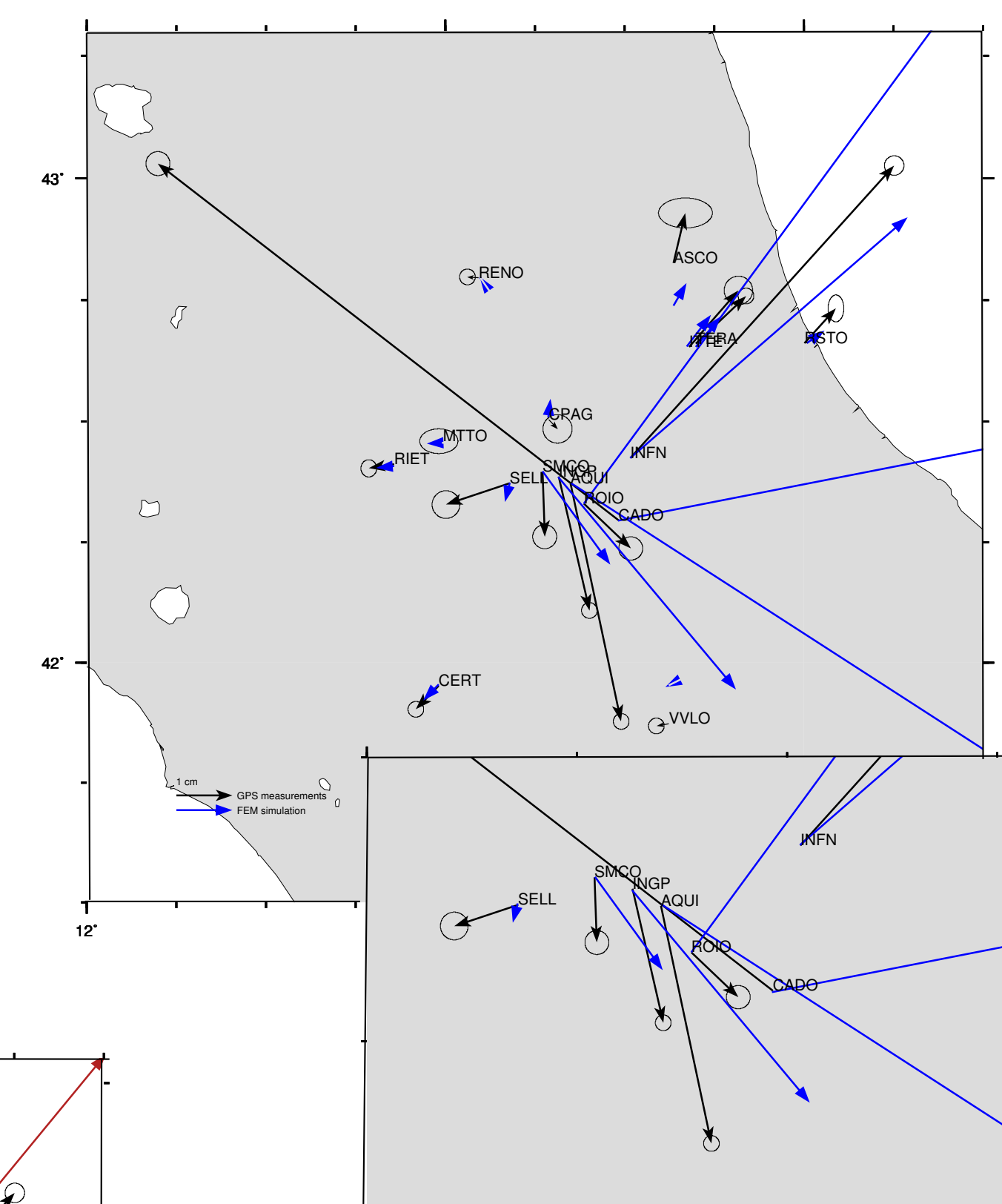
strike angle=142.°
dip angle=42.°
rake angle= variable

WORK
IN PROGRESS

4



RESULTS



The calculated coseismic displacement
field is compared with GPS measurements
from Anzidei et al. 2009.

3D plots of the horizontal
and vertical deformation
field obtained with source 3
(Atzori et al. 2009).

